

# CLIC Beam Delivery System

- (1) Parameters & Perspective
- (2) Final Focus
  - Goal, Layout, Constraints, Options
- (3) Collimation
  - Requirements & Problems
- (4) IP Region and Exit Line
  - Spent Beam, Debris, Crossing Angle

# (1) Parameters & Perspective

parameter	symbol	SLC	NLC	CLIC
<b>c.m. energy [TeV]</b>	$E$	<b>0.1</b>	1	<b>3</b>
<b>luminosity [<math>10^{34}</math> cm<math>^{-2}</math> s<math>^{-1}</math>]</b>	$L$	<b>0.0002</b>	1.3	<b>10</b>
repetition rate [Hz]	$f_{rep}$	120	120	100
bunch charge [ $10^{10}$ ]	$N_b$	3.7	1	0.4
bunches/rf pulse	$n_b$	1	95	154
bunch separation [ns]	$\Delta_b$	—	2.8/1.4	0.67
av. beam power [MW]	$P_b$	0.04	9	14.8

parameter	symbol	SLC	NLC	CLIC
<b>IP hor. emittance [<math>\mu\text{m}</math>]</b>	$\gamma\epsilon_x$	<b>50</b>	4.5	<b>0.68</b>
<b>IP vert. emittance [<math>\mu\text{m}</math>]</b>	$\gamma\epsilon_y$	<b>8</b>	0.1	<b>0.02</b>
hor. beta [mm]	$\beta_x^*$	2.8	12	8
vert. beta [mm]	$\beta_y^*$	1.5	0.15	0.15
<b>hor. spot size [nm]</b>	$\sigma_x^*$	<b>1700<sup>†</sup></b>	235	<b>43</b>
<b>vert. spot size [nm]</b>	$\sigma_y^*$	<b>900<sup>†</sup></b>	4	<b>1.0</b>
bunch length [mm]	$\sigma_z$	1	0.12	0.03
<b>Upsilon</b>	$\Upsilon$	$2 \times 10^{-3}$	0.3	<b>8.1</b>
pinch enhancement	$H_D$	2.0	1.45	2.24
<b>beamstrahlung</b>	$\delta_B$ [%]	<b>0.06</b>	10	<b>31</b>
photons per $e^-$ ( $e^+$ )	$N_\gamma$	1	1.4	2.3

<sup>†</sup> 1998 average value

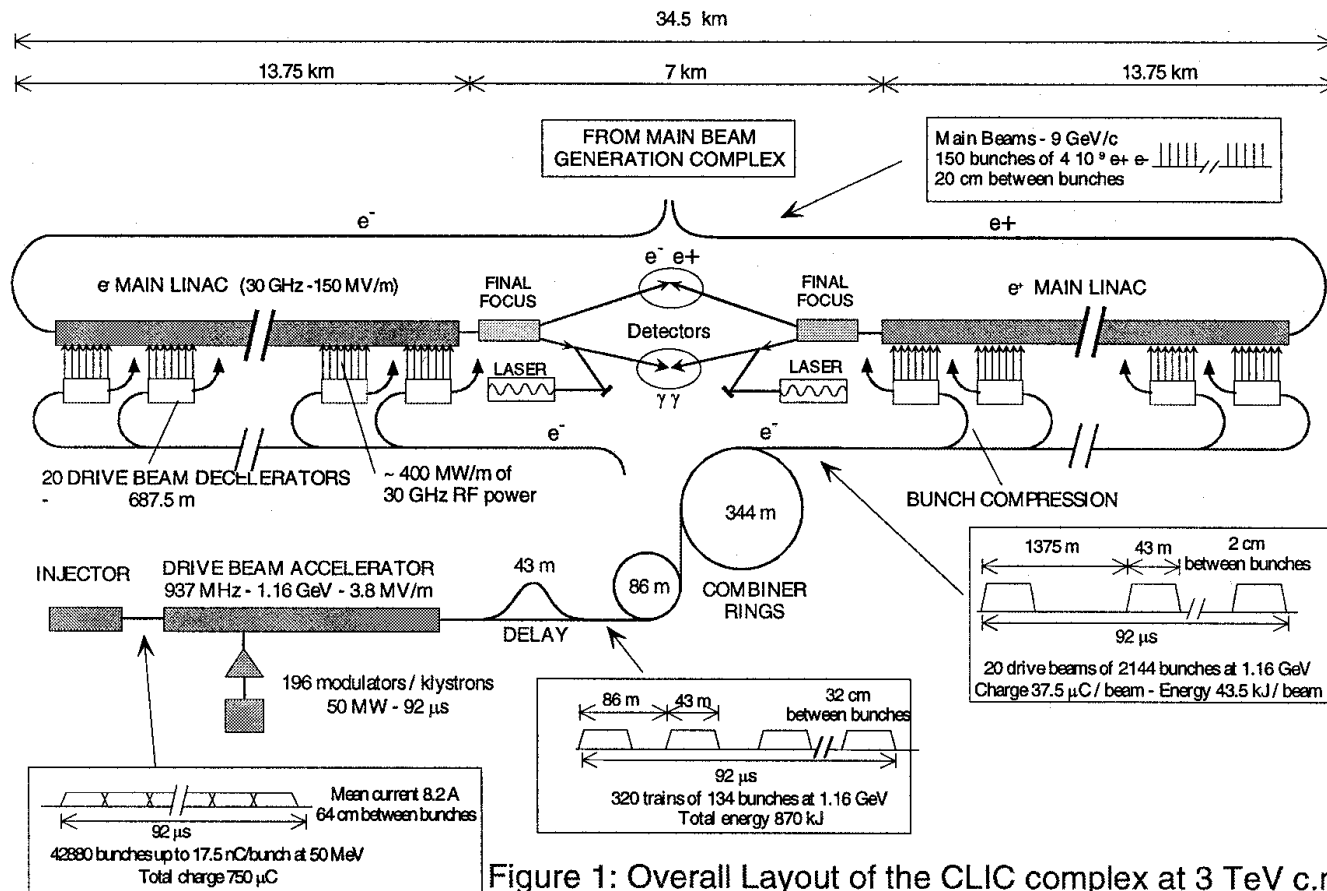
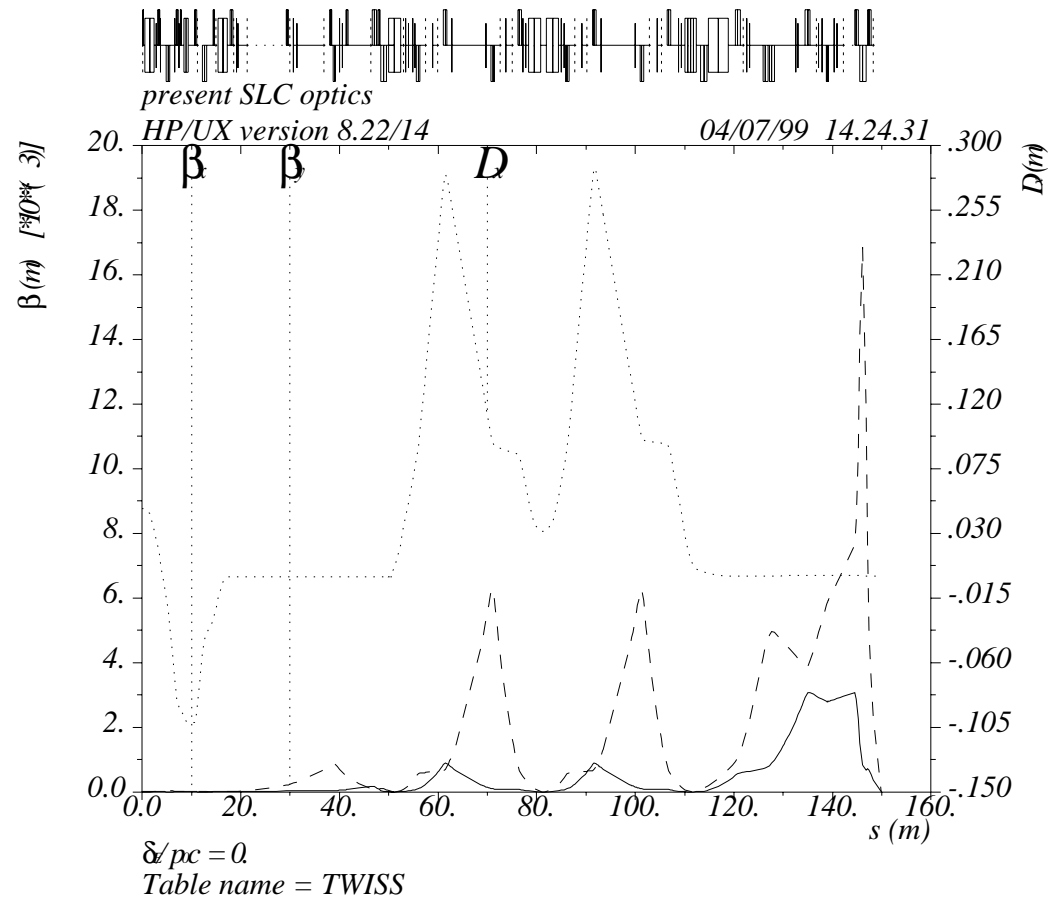
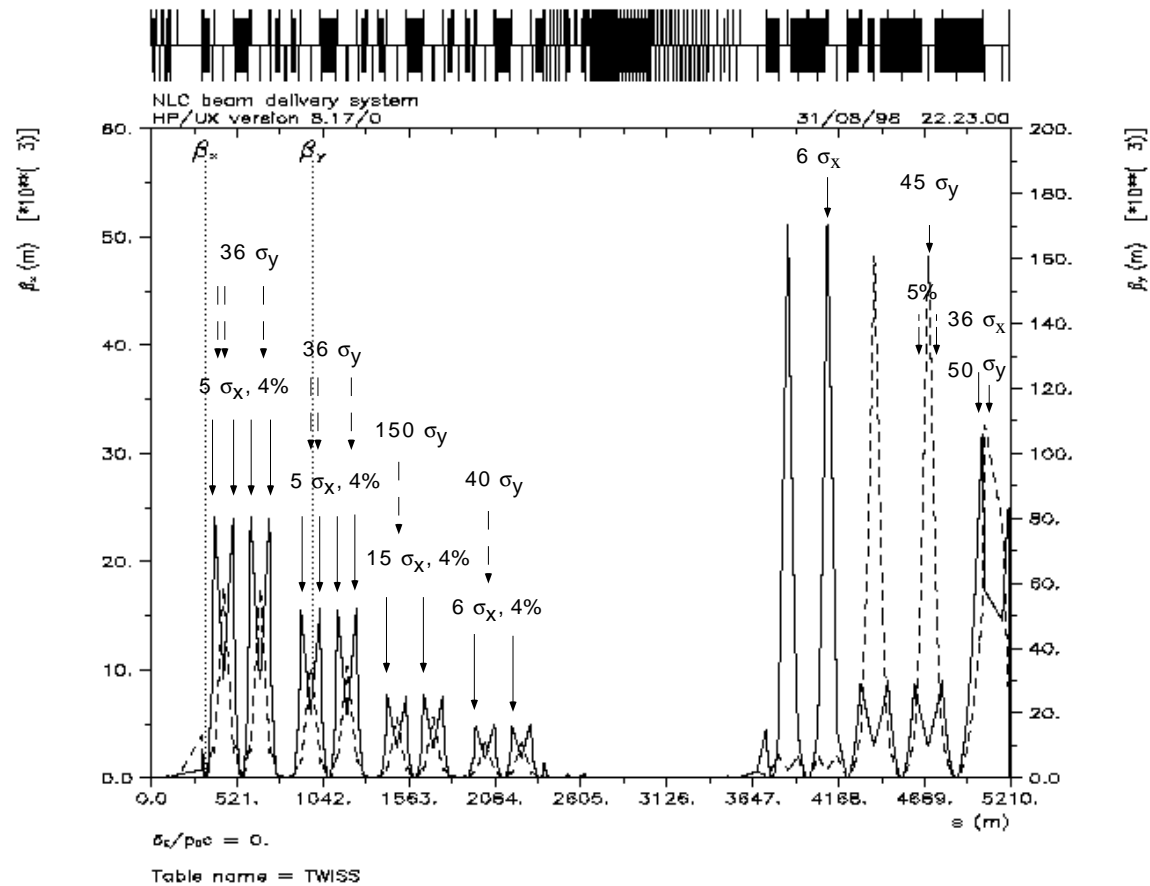


Figure 1: Overall Layout of the CLIC complex at 3 TeV c.m.

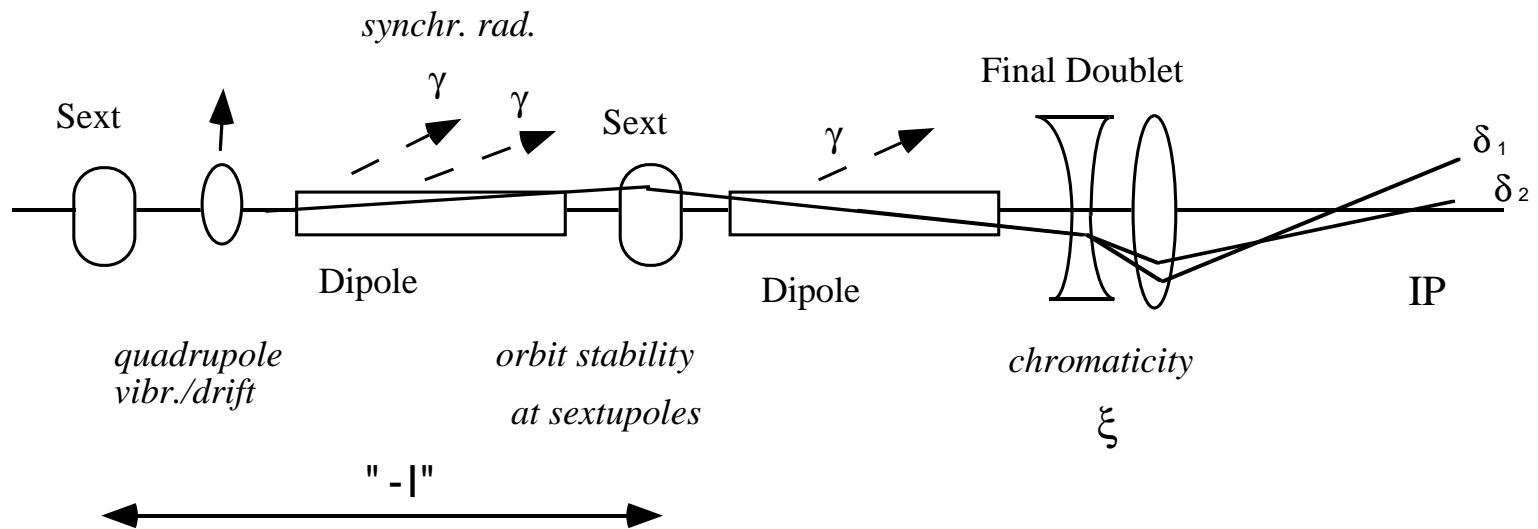


Optics of the SLC beam delivery system for 50-GeV beam energy.  
 Total length (per side) is 150 m.



Optics of the NLC beam delivery system for 500-GeV maximum beam energy. Total length (per side) is 5 km.

# (2) Final Focus



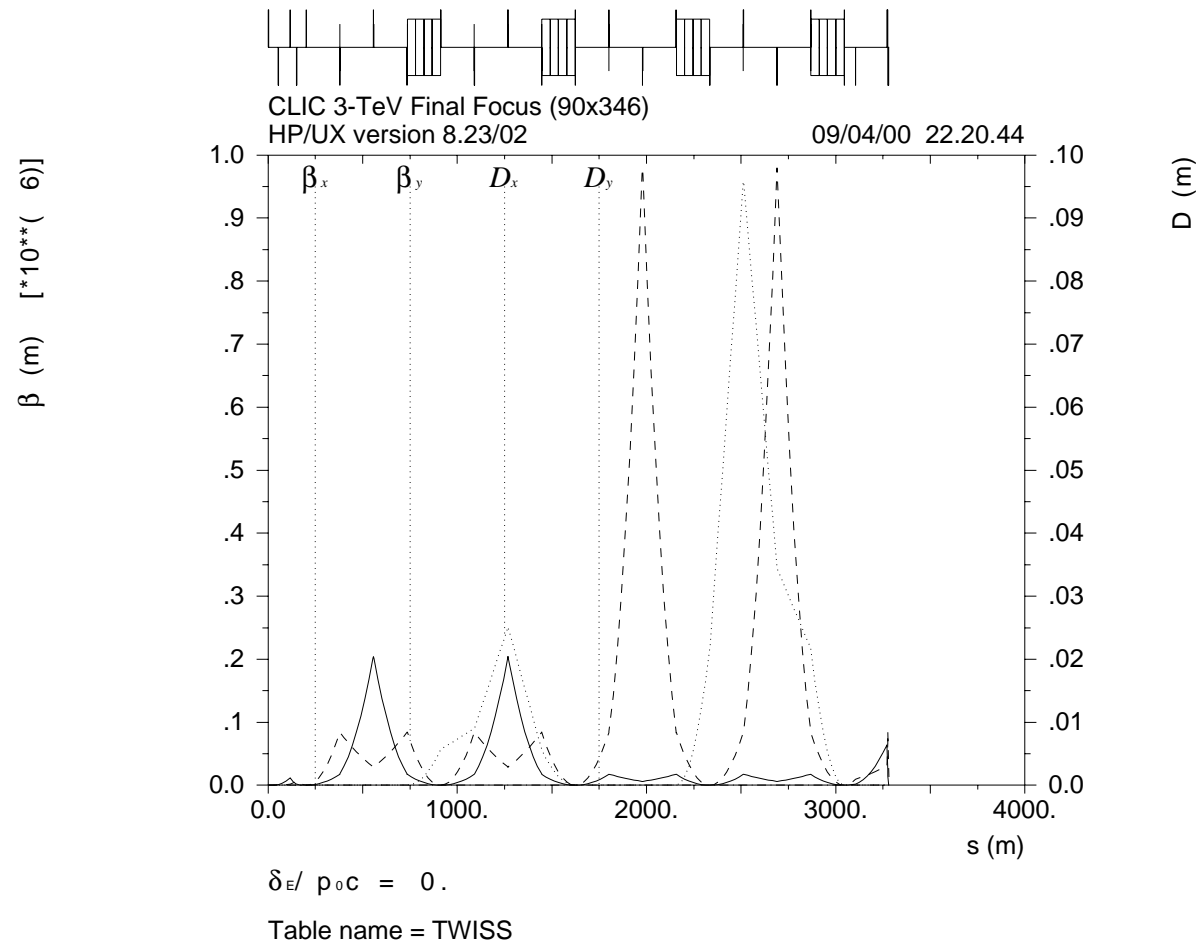
Schematic of a conventional final focus.

# Approaches

- 4 sextupoles for chromatic correction; **standard arrangement**: SX1, SX2, SY1, SY2, with  $-I$  transform between the two horizontal and the two vertical sextupoles.
- **interleaved sextupoles** (SLC): SX1, SY1, SX2, SY3; saves space, more aberrations.
- **Oide's odd dispersion scheme**: standard sequence, but  $\eta_x$  only at SX2 and SY2. Advantages: fewer bends and less aberrations.
- **Brinkmann sextupoles**, to compensate for the chromatic breakdown of the  $-I$ .
- **Raimondi scheme**:  $\eta'_x$  at the IP, and sextupoles near final doublet, extremely compact, tuning more difficult?
- **rf quadrupoles**: use correlation of energy and  $z$  within bunch; if addition to conventional scheme, rf dipoles are also needed, to bump the orbit across the sextupoles.

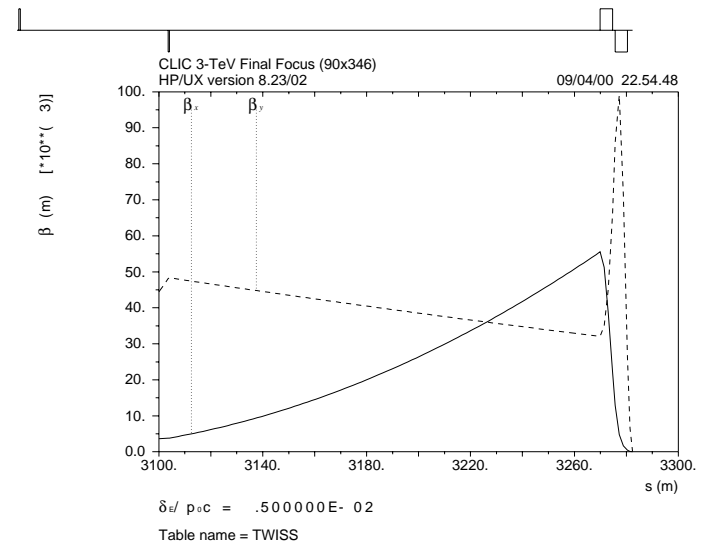
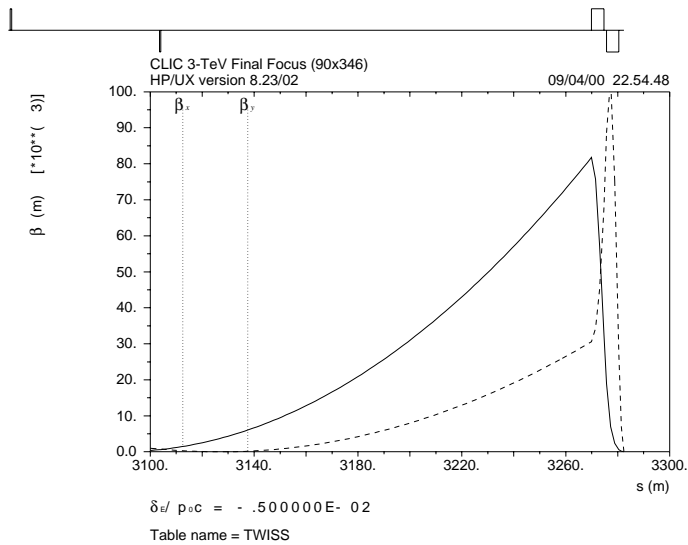
# Draft Optics

- baseline design, aided by FFADA code and O. Napoly
- beta match, chromatic correction (CCX, CCY) and final transformer, total demagnification factor 90/346, initial  $\beta_{x,y} \sim 65, 18$  m
- odd-dispersion scheme à la Oide  $\rightarrow$  fewer dipoles, larger bandwidth
- final-quadrupole gradient: 450 T/m, extrapolating from LHC magnet design: 320 T/m & 35 mm 1/2 inner radius
- trade-off between Oide effect ( $\rightarrow$  large  $\xi_x$ ) and chromatic bandwidth ( $\rightarrow$  small  $\xi_x$ )
- vary bending/drift lengths, ratio vertical/horizontal bending angle, strength of final-doublet quadrupoles, Brinkmann sextupoles,... for optimum luminosity with 1% flat energy spread



Final-focus optics: beta functions and (odd) dispersion.

# Chromatics: $d\beta/d\delta$



Final-telescope optics for energy offsets of  $-0.5\%$  and  $+0.5\%$ .

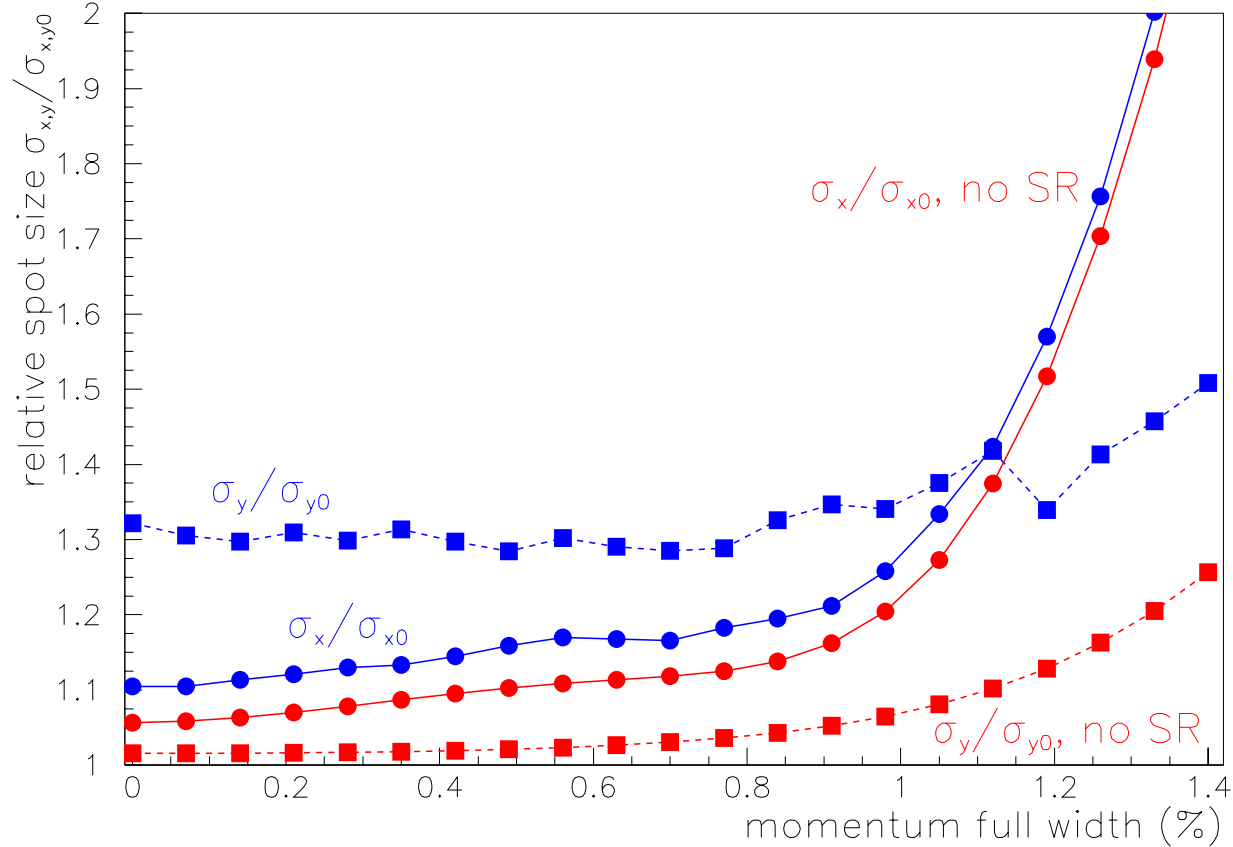
# Final-focus characteristics

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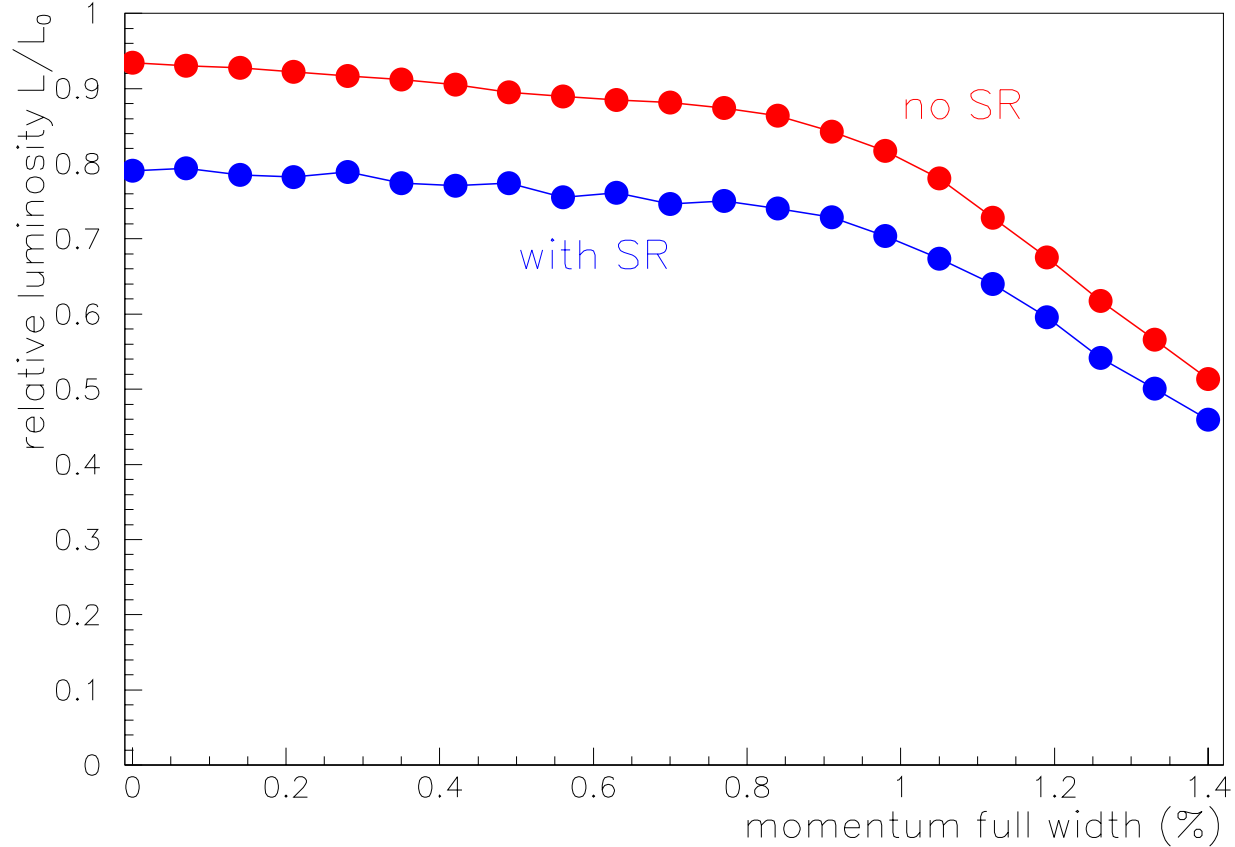
total length (per side)	3282 m
demagnification factor $M_{x,y}$	90, 346
IP beta functions $\beta_{x,y}^*$	8, 0.15 mm
FT chromaticity $\xi_{x,y}$	6900, 27000 <sup>†</sup>
bending length	4×176 m
angle per dipole section	63, 230 $\mu$ rad
final quadrupole gradient	450 T/m
beta function $\hat{\beta}_y$ at CCY sextupoles	1000 km <sup>†</sup>
peak dispersion $\eta_x$ in CCY	0.1 m <sup>†</sup>
beta functions $\beta_{x,y}$ at entrance to final quad	15, 88 km

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<sup>†</sup> NLC:  $\xi_x \approx 7000$ ,  $\xi_y \approx 30000$ ,  $\hat{\beta}_y \approx 200$  km,  $\eta_x \approx 0.1$  m

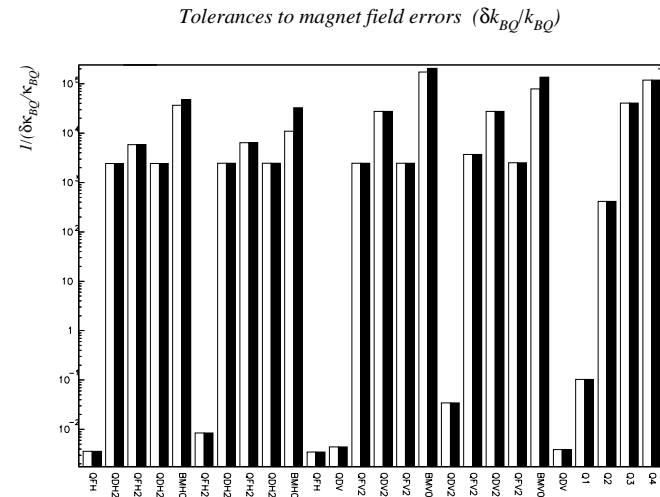
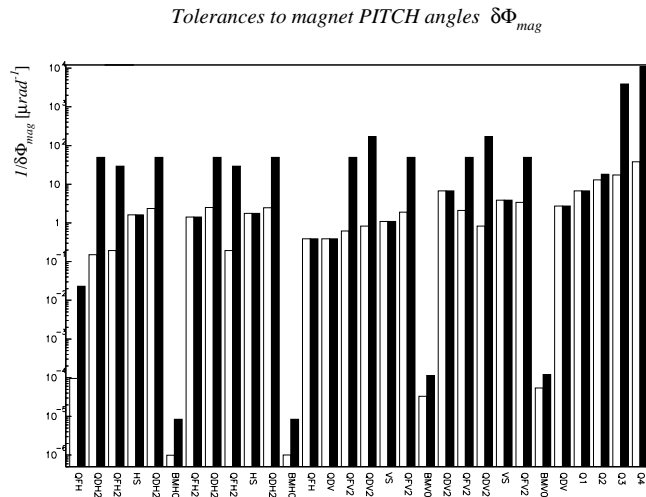


Relative rms spot sizes versus the full energy spread for a flat distribution. Design spot sizes:  $\sigma_{x0} = 43$  nm,  $\sigma_{y0} = 1.0$  nm.



Relative luminosity (from tracking & convolving) vs. energy spread.  
 Ideal luminosity w/o pinch:  $L_0 = 4.6 \times 10^{34} \text{ cm}^{-2}\text{s}^{-1}$ .





Sensitivities to pitch angle (left) and relative field change  $\Delta k_{BQ}/k_{BQ}$  (right), again calculated with FFADA. The tightest pitch angle tolerance is 0.1 nrad for the final quadrupole. Field stability tolerances are about  $10^{-5}$ .

### (3) Collimation System

2 functions: halo removal & machine protection

major problem: collimator survival for bunch train impact

$$\sigma_{UTS} > \frac{\alpha E}{C_p} \frac{d\mathcal{E}}{dm}$$

with  $\sigma_{UTS}$  ultimate tensile strength,  $\alpha$  linear thermal expansion coefficient,  $C$  heat capacity,  $E$  elastic modulus,  $d\mathcal{E}/dm$  energy loss per g material. Rewrite this as

$$\sigma_x \sigma_y > \frac{\alpha E}{\sigma_{UTS} C_p} \frac{d\mathcal{E}}{dx} \left( \frac{n_b N_b}{2\pi} \right)$$

E.g., copper,  $\alpha = 1.7 \times 10^{-5} \text{ K}^{-1}$ ,  $E = 120 \text{ GPa}$ ,  $C_p = 0.385 \text{ Jg}^{-1}\text{K}^{-1}$ ,  $d\mathcal{E}/dx \approx 1.44 \text{ MeV cm}^2/\text{g}$ ,  $\sigma_{UTS} = 300 \text{ MPa}$ :

$$(\sigma_x \sigma_y)^{1/2} > 200 \text{ } \mu\text{m} \quad \text{or} \quad \beta_{x,y} \geq 1000 \text{ km}$$

# Collimator Materials

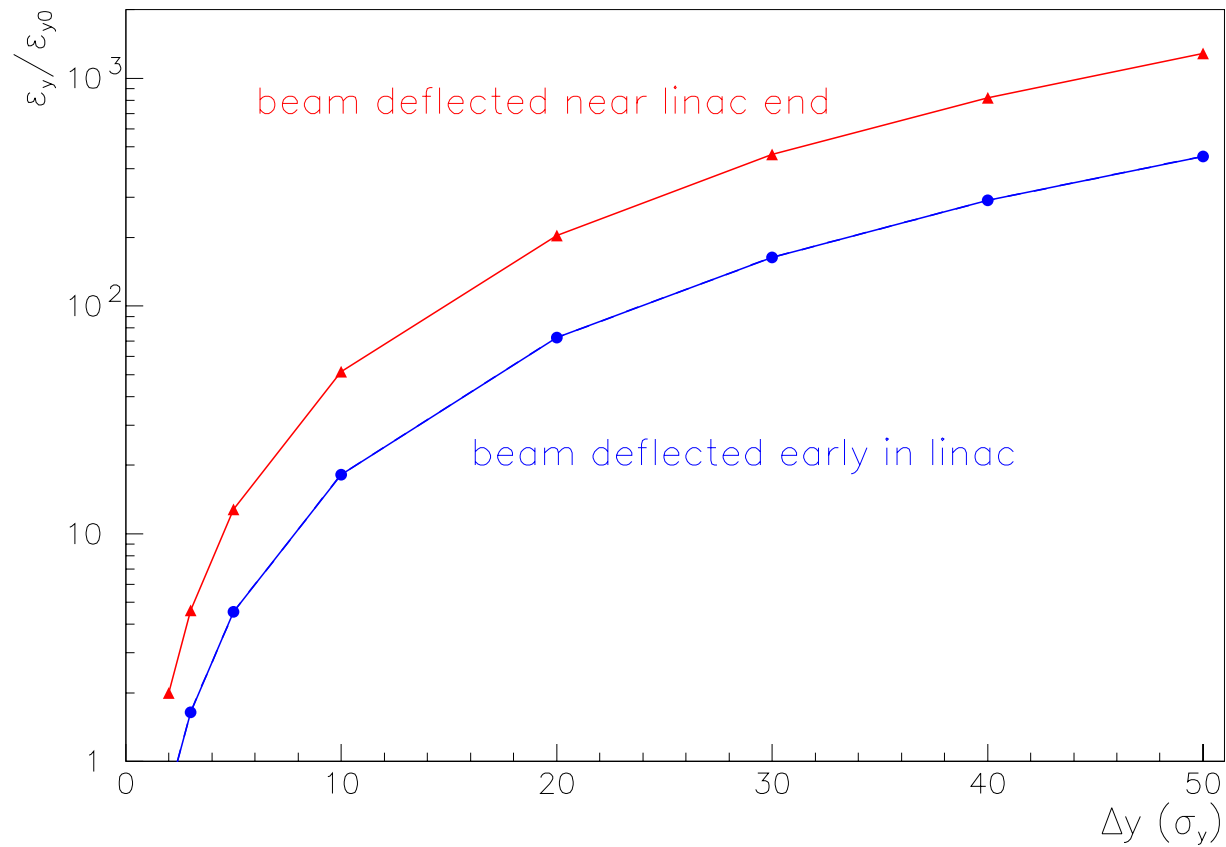
material	$\alpha$	$E$	$C_p$	$c_p$	K	$\sigma$	$\sigma_{\min}$
	[1/K]	[GPa]	[ $\frac{\text{J}}{\text{gK}}$ ]	[ $\frac{\text{MJ}}{\text{m}^3\text{K}}$ ]	[ $\frac{\text{W}}{\text{Km}}$ ]	[ $\Omega^{-1}\text{m}^{-1}$ ]	[ $\mu\text{m}$ ]
Cu	16.5	120	0.385	3.4	390	$6 \times 10^7$	200
Ti	8.5	110	0.52	2.4	17	$2 \times 10^6$	100
W	4.4	411	0.132	6.8	200	$2 \times 10^7$	84

Other parameters  $dE/dx \approx 1.14 - 1.51 \text{ MeV cm}^2/\text{g}$  and  $\sigma_{\text{UTS}} \approx 300 - 400 \text{ MPa}$ .

In present final-focus design, maximum spot sizes are  $\sqrt{\sigma_x \sigma_y} \approx 45 \mu\text{m}$  at the first three sextupoles,  $\sqrt{\sigma_x \sigma_y} \approx 76 \mu\text{m}$  for the last one.

# emittance growth of mis-steered beam

(PLACET, D. Schulte)



## Fundamental Questions:

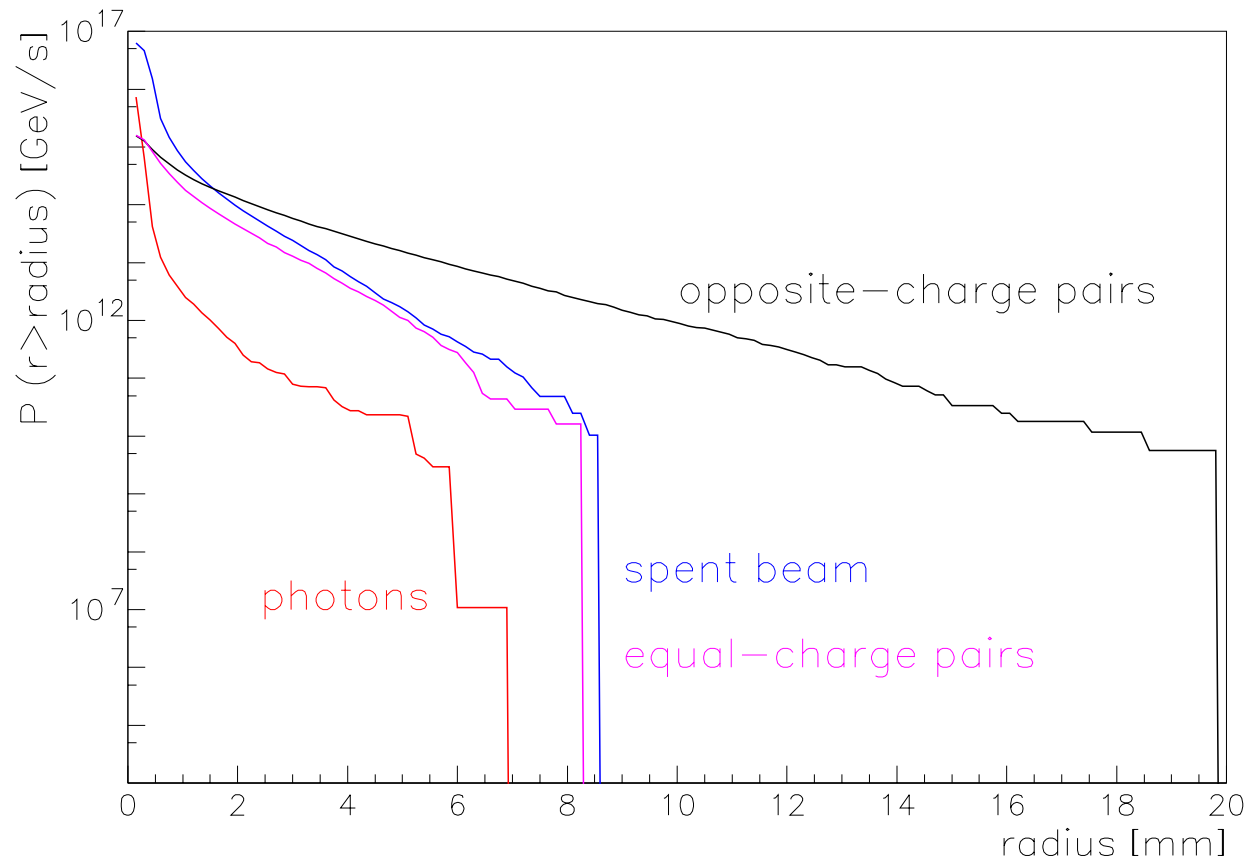
- how much halo do we expect?
- how many muons per bunch train are acceptable for the detector?
- which are the failure modes in the linac that can missteer the beam? what is the emittance increase as a function of linac steering error?

We hope that collimation only in the final focus will be sufficient, and that we do not need beta function as large as naively estimated.

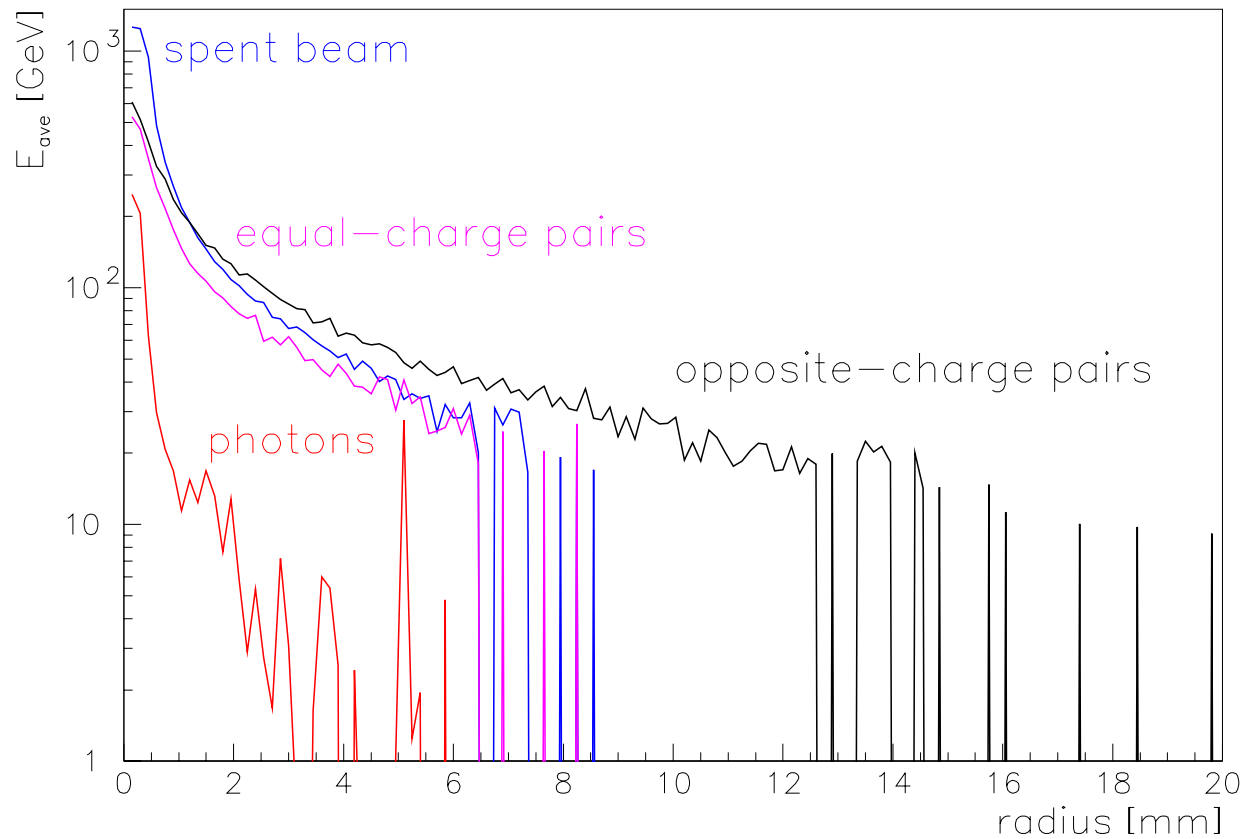
## (4) IP and Exit Line Issues

- *background from coherent pairs and beamstrahlung*; at 3 TeV there are about as many pairs as beam particles!
- *extraction of spent beam with  $\Delta E/E \approx 100\%$* , photons and pairs, layout of final quadrupole
- suppression of *thermal shock waves* (J.B. Jeanneret)
- exit line diagnostic, luminosity monitors, tuning
- effects of solenoid field, multibunch kink instability, crab crossing (O. Napoly)
- *off-center collisions in the high- $\Upsilon$  regime*: angular divergence, beamstrahlung, defl. scans (Napoly)

spent beam & debris 2 meters from IP:  
power at  $r > a$   
(D. Schulte, Guinea-Pig)



spent beam & debris 2 meters from IP:  
average energy  
(D. Schulte, Guinea-Pig)



# Crossing Angle

## Constraints

- **loss in luminosity** (w/o crab):  $L/L_0 \approx 1/\left(\sqrt{1 + \left(\frac{\phi_c}{2\phi_d}\right)^2}\right)$   
where  $\phi_d = \sigma_x/\sigma_z \approx 1.4$  mrad, e.g.,  $L/L_0 = 28\%$  for  $\phi_c = 10$  mrad, and  $14\%$  for  $\phi_c = 20$  mrad.
- **multi-bunch kink instability:**  
 $\phi_c \geq \sqrt{D_x m_b} (3D_y)^{1/4} \phi_d \approx 12$  mrad, with  $m_b = 154$  no. of bunches;  $D_x = 2N_b r_e \sigma_z / (\gamma(\sigma_x + \sigma_y)\sigma_x) = 0.12$ ,  $D_y = 5.2$ ; simulations indicate that 10 mrad would be ok (O. Napoly).
- **space for spent beam & collisions debris**, in particular for **opposite-charge pairs** (D. Schulte).

# Crab Crossing

Crab cavity produces  $z$ -dependent displacement at IP:

$$\frac{\partial x^*}{\partial z} = \frac{\phi_c}{2}$$

or

$$\frac{\phi_c}{2} = R_{12} \frac{eV_{\max} k_{\text{rf}}}{E}$$

where  $R_{12} \approx 23$  m;  $\rightarrow V_{\max} = 1$  MV at 30 GHz.

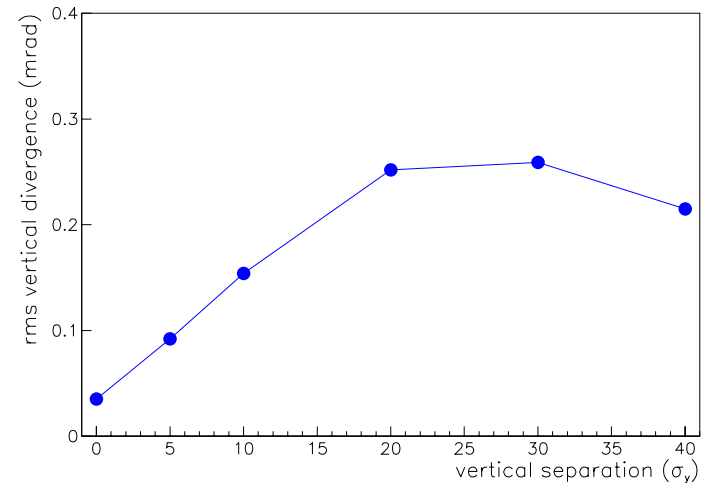
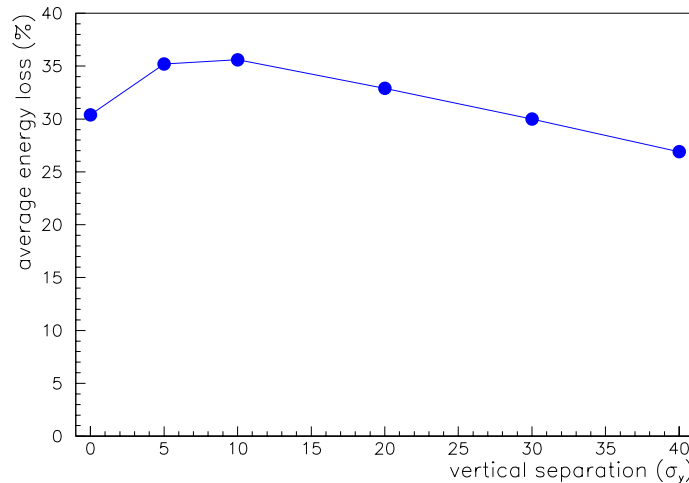
If relative phase of crab cavities jitters, the collision will not be head-on. **Tolerance** for 2% luminosity loss:

$$\Delta z \leq \frac{4}{5} \frac{\sigma_x}{\phi_c} \quad \text{or} \quad \Delta\phi_{\text{rf}} \leq k_{\text{rf}} \frac{4}{5} \frac{\sigma_x}{\phi_c} \approx 0.06^\circ$$

at 30 GHz. Tighter at lower frequencies.

For comparison: **KEKB crab cavities**, 500 MHz,  $\phi_c = 11$  mrad,  $\sigma_x = 200$   $\mu\text{m}$ :  $\Delta\phi_{\text{rf}} \leq 8^\circ$ , much relaxed.

# Off-Center Collisions at High- $\Upsilon$



Average relative energy loss (left) and rms divergence of spent beam (right) vs. vertical beam-beam separation, as simulated with GUINEA-PIG. Incoming divergences:  $\theta_{x,y}^* \approx 5 - 7 \mu\text{rad}$ , characteristic deflection angle:  $\theta_d = 2N_b r_e / (\gamma(\sigma_x + \sigma_y)) \approx 170 \mu\text{rad}$ .  
Exit line acceptance should suffice for off-center collisions!

## (5) Summary

- 3-km long baseline final-focus optics exists;  
 $L/L_0 \approx 70 - 80\%$  with  $\Delta E/E|_{FW} \approx 1\%$ ; compromise between SR in last quadrupole and higher-order chromatics; now exploring shorter alternatives
- jitter tolerance of  $Q1$ :  $\Delta y < 0.2$  nm, determined by  $\sigma_y^*$
- collimation profits from increased emittance of missteered beam; integrated in FF; det. requirements?
- crossing angle  $\phi_c \geq 20$  mrad,  $\Delta\phi_{rf} < 0.06^\circ$  at 30 GHz.
- spent-beam disposal & extraction line diagnostics: still to be studied